JC18 Rec'd PCT/PTO 0 7 DEC 2001

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•	RANSMITTAL LETTER	942640-18							
1	DESIGNATED/ELECT	U.S. APPLICATION NO (If known, see 37 CFR 1.5							
•	CONCERNING A FILIN	N/A10/009542							
INTERN	IATIONAL APPLICATION NO.	INTERNATIONAL FILING DATE	PRIORITY DATE CLAIMED						
	/EP00/05364	June 9, 2000	June 9, 1999						
	TITLE OF INVENTION FACILITY FOR THE GASIFICATION OF CARBON-CONTAINING FEED MATERIALS								
	APPLICANT(S) FOR DO/EO/US KARL, Jurgen								
	Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:								
	577								
		NT submission of items concerning a filing t	ander 35 U.S.C. 371.						
3. [x] '	This is an express request to begin r	national examination procedures (35 U.S.C. 3							
	items (5), (6), (9) and (21) indicated The US has been elected by the exp	iration of 19 months from the priority date (A	Article 31).						
	A copy of the International Applica	tion as filed (35 U.S.C. 371(c)(2))							
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		y the International Bureau.	ring Office (RO/US)						
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6. X		the International Application as filed (35 U.S	5.C. 3/1(C)(2)).						
	a.	nitted under 35 U.S.C. 154(d)(4).							
		nternational Aplication under PCT Article 19	(35 U.S.C. 371(c)(3))						
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		ever, the time limit for making such amenda	nents has NOT expired.						
	d. A have not been made and								
8.	An English language translation of	the amendments to the claims under PCT Ar	ticle 19 (35 U.S.C. 371 (c)(3)).						
9. 🗌	An oath or declaration of the inven	ator(s) (35 U.S.C. 371(c)(4)).							
10. An English lanugage translation of the annexes of the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(c)(5)).									
Iten	ns 11 to 20 below concern docume	ent(s) or information included:							
11.		ment under 37 CFR 1.97 and 1.98.							
12.	An assignment document for rec	ording. A separate cover sheet in compliance	e with 37 CFR 3.28 and 3.31 is included.						
13. 🛮	A FIRST preliminary amendmen	nt.							
14.	A SECOND or SUBSEQUENT	preliminary amendment.							
15.	A substitute specification.								
16.	A change of power of attorney as								
17.	A computer-readable form of the	e sequence listing in accordance with PCT Ru	ile 13ter.2 and 35 U.S.C. 1.821 - 1.825.						
18.	A second copy of the published	international application under 35 U.S.C. 154	4(d)(4).						
19.	19. A second copy of the English language translation of the international application under 35 U.S.C. 154(d)(4).								
20.	Other items or information:								

U.S. APPLICATION NO (16 APPLICATION NO PCT/EP00/05364					ATTORNEY'S DOCKET NUMBER 942640-18				
						CALCULATIONS PTO USE ONLY			
	21. X The following fees are submitted: BASIC NATIONAL FEE (37 CFR 1.492 (a) (1) - (5)):								
Neither international preliminary examination fee (37 CFR 1.482) nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO and International Search Report not prepared by the EPO or JPO									
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b. Please charge my Deposit Account No in the amount of \$ to cover the above fees. A duplicate copy of this sheet is enclosed.									
c. X The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. 50-0639. A duplicate copy of this sheet is enclosed.									
d. Fees are to be charged to a credit card. WARNING: Information on this form may become public. Credit card information should not be included on this form. Provide credit card information and authorization on PTO-2038.									
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NOTE: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137 (a) or (b)) must be filed and granted to restore the application to pending status									
SEND ALL CORRESPONDENCE TO.									
Brian M. B	erliner			SIGNATU	JRE		_ _		
)		Brian	n M.	Berliner			
O'Melveny & Myers LLP 400 South Hope Street NAME									
Los Angeles, CA 90071-2899 34,549									
REGISTRATION NUMBER									

JC13 Rec'd PCT/PTO 0 7 DEC 2001

EXPRESS MAIL: EL870079432US

PATENT 942640-18

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

Applicant: KARL, Jürgen

Art Unit:

Serial No.:

Examiner:

Filed:

LXamme

Title: Facility for the Gasification of Carbon-

Containing Feed Materials

PRELIMINARY AMENDMENT

United States Patent and Trademark Office Assistant Commissioner for Patents BOX PCT P.O. Box 2327 Arlington, Virginia 22202

Sir:

Preliminary to examination, please amend the above-identified patent application as follows:

IN THE SPECIFICATION:

Please amend the specification as follows:

On page 1, line 3, following the title, please insert:

BACKGROUND OF THE INVENTION

On page 3, before the paragraph beginning on line 12, please insert:

<u>SUMMARY OF THE INVENTION</u>

On page 3, delete the paragraph beginning on line 22.

Please replace the paragraph beginning on page 5, line 13, with the following rewritten paragraph:

In an embodiment of the invention, the fluidized-bed gasification chamber is arranged, in spatial terms, above the filter chamber and the filter chamber is arranged above the combustion chamber. This arrangement results in a very compact construction with a good energy balance.

Please replace the paragraph beginning on page 5, line 20, with the following rewritten paragraph:

In another embodiment of the invention, there is provided an additional heat exchanger, which takes up the waste heat of the drawing-off flue gas and gives it off to the product gas, this likewise improving the energy balance.

Please replace the paragraph beginning on page 5, line 26, with the following rewritten paragraph:

In another embodiment of the invention, heat-exchanger ribs are arranged on the heat-exchanger sections of the heat pipes. These ribs are formed so as to assume an operative relationship with the streams and vortices of fluid produced by the fluidizing arrangements, such that the fluidized particles are accelerated transversely to their original flow direction. It is thus the case that good transverse mixing of the fluidized bed

is achieved, the residence time of the particles in the fluidized bed is increased, gas bubbles are well dispersed, and the heat transfer from the heat-exchanger ribs to the fluidized bed is improved to a considerable extent. This also makes it possible to achieve a compact construction.

Please replace the paragraph beginning on page 6, line 1, with the following rewritten paragraph:

A fluidized-bed reactor in accordance with the invention is particularly suitable for use in a facility for producing combustible gas from carbon-containing feed materials according to the present invention. A reactor vessel which accommodates the fluidized bed is provided in the fluidized-bed reactor. Fluidizing arrangements for fluidizing a predetermined region of the fluidized bed are provided. In order for additional heat to be introduced or drawn off in this region, use is made of heat exchangers. The better the heat transfer between the heat exchangers and the fluidized bed, the higher is the efficiency of the installation. In order to improve this heat transfer, the heat-exchanger sections of the heat exchanger are designed as special heat-exchanger ribs which are formed and arranged so as to assume an operative relationship with the streams and vortices of fluid produced by the fluidizing arrangements, such that the fluidized particles are accelerated transversely to their original flow direction, as a result of which the transverse mixing of the fluidized bed is improved, the residence time of the particles in the fluidized bed is increased, and the heat transfer from the heat-exchanger ribs to the fluidized bed is improved to a considerable extent.

On page 7, delete the paragraph beginning on line 8.

Please replace the paragraph beginning on page 7, line 12, with the following rewritten paragraph:

In another embodiment of the invention, the heat-exchanger ribs are connected releaseably to the heat-exchanger sections. This embodiment has a series of advantages: since, for example, fluidized beds in which combustion processes take

place, on account of the relatively high temperature in conjunction with the sand of the fluidized bed, have a highly abrasive effect on internals, the heat-exchanger ribs are particularly effected thereby, i.e. they are subject to a high level of wear. The exchangeability of these parts which are subject to wear is thus particularly cost-effective.

Please replace the paragraph beginning on page 7, line 24, with the following rewritten paragraph:

In yet another embodiment of the invention, heat pipes are used. It is clear to the person skilled in the art that the positive effect provided by the invention is merely achieved by the particular configuration of the heat-exchanger ribs in conjunction with the fluidized bed. The combination of the special heat-exchanger ribs with heat pipes again allows a reduced overall size for maintaining the same output.

On page 7, before the paragraph beginning on line 33, please insert:

BRIEF DESCRIPTION OF THE DRAWINGS

On page 8, before the paragraph beginning on line 21, please insert:

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

IN THE ABSTRACT:

Please insert the abstract of the disclosure as follows:

ABSTRACT

A pressure-supercharged fluidized-bed gasification chamber has a pressure-tight lock for supplying the feed materials which are to be gasified. The fluidized-bed gasification chamber is connected to a filter chamber via a connecting channel, with the result that the gas produced can flow over from the fluidized-bed gasification chamber into the filter chamber, where it is directed through the filter layer. An external heat source provides the necessary heat for the allothermic gasification. A heat-pipe arrangement directs the heat from the external heat source into the gasification bed of the fluidized-bed gasification chamber, in order to provide the temperature which is necessary for the gasification.

IN THE CLAIMS:

Please amend Claims 1-14 as follows:

- 1. (Amended) A facility for producing combustible gas from carbon-containing biogenic feed materials by allothermic steam gasification, the facility comprising:
- a pressure-supercharged fluidized-bed gasification chamber with a pressure-tight lock for supplying the feed materials that are to be gasified,
- a filter chamber connected to the fluidized-bed gasification chamber via a connecting channel,

an external heat source, and

- a heat-pipe arrangement that takes up heat from the external heat source and gives it off to the gasification bed in the fluidized-bed gasification chamber.
- 2. (Amended) The facility as claimed in claim 1, wherein the external heat source further comprises a fluidized-bed combustion chamber and has a flue-gas discharge line.
- 3. (Amended) The facility as claimed in claim 2, wherein the fluidized-bed combustion chamber is connected to the filter chamber via a solids flow channel that is directed upward to the filter chamber,

wherein the solids flow channel has a bottom end section connected to the combustion chamber,

wherein the solids flow channel has a top end section connected to the filter chamber, and

wherein a siphon arrangement is arranged at the bottom end section.

4. (Amended) The facility as claimed in claim 3, wherein a first blowing arrangement is arranged in the bottom end section by use of suction action, in a controlled manner, for solids to be drawn off into the fuel bed of the combustion chamber from the filter bed of the filter chamber, with pulsating action.

- 5. (Amended) The facility as claimed in claim 4, wherein a second blowing arrangement is arranged in the top end section of the solids flow channel or in the filter chamber in order to rearrange and/or loosen the filter bed of the filter chamber in a controlled manner.
- 6. (Amended) The facility as claimed in claim 2, wherein a flue-gasregulating arrangement is provided in the flue-gas discharge line in order to adjust the ratio of flue gas to product gas.
- 7. (Amended) The facility as claimed in claim 1, wherein the fluidized-bed gasification chamber is arranged above the filter chamber and the filter chamber is arranged above the combustion chamber.
- 8. (Amended) The facility as claimed in claim 2, further comprising an additional heat exchanger, which takes up the waste heat of the drawing-off flue gas and gives it off to the product gas.
- 9. (Amended) The facility as claimed in claim 1, wherein heat-exchanger sections of the heat-pipe arrangement have heat-exchanger ribs which are formed and arranged so as to assume an operative relationship with the streams and vortices of fluid produced by the fluidizing arrangements, such that fluidized particles are accelerated transversely to their original flow direction, as a result of which transverse mixing of the fluidized bed is improved, the residence time of the particles in the fluidized-bed is increased, gas bubbles are well dispersed, and heat transfer from the heat-exchanger ribs to the fluidized-bed is improved to a considerable extent.
- 10. (Amended) A fluidized-bed reactor, comprising:
 a reactor vessel for accommodating a fluidized bed, which is fluidized in a region by fluidizing means, and

heat exchangers with heat-exchanger sections arranged in the fluidized region, wherein heat-exchanger ribs are formed and arranged on the heat-exchanger sections of the heat exchangers so as to assume an operative relationship with the streams and vortices of fluids produced by the fluidizing means, such that the fluidized particles are accelerated transversely to their original acceleration direction, as a result of which the transverse mixing of the fluidized bed is improved, the residence time of the fluidized particles in the fluidized bed is increased, gas bubbles are well dispersed, and the heat transfer from the heat-exchanger ribs to the fluidized bed is improved to a considerable extent.

- 11. (Amended) The fluidized-bed reactor as claimed in claim 10, wherein the heat-exchanger ribs are of helical or blade-like design.
- 12. (Amended) The fluidized-bed reactor as claimed in claim 10, wherein, on horizontally located heat-exchanger sections, the heat-exchanger ribs are inclined obliquely to the blowing direction of the fluidizing means, the direction of inclination of the heat-exchanger ribs differing from adjacent heat-exchanger sections.
- 13. (Amended) The fluidized-bed reactor as claimed in claim 12, wherein the heat-exchanger ribs are connected releaseably to the heat-exchanger sections, the connection providing good heat transfer.
- 14. (Amended) The fluidized-bed reactor as claimed in claim 10, wherein the heat exchangers have heat pipes.

REMARKS

Claims 1-14 are pending in this application, as amended above. The Applicant has amended the claims to place them in better condition for examination. Also, the Applicant has amended the specification, and has added an Abstract. It is noted that the amendments to the specification refer to page and line numbers as set forth in the attached English translation of the present application. No new matter has been added to the application by this preliminary amendment. Accordingly, the Applicant respectfully requests an examination of the application on the merits in view of the foregoing amendments.

Attached hereto is a marked-up version of the changes made to the specification and claims by the current amendment. The attached page is captioned "Version with markings to show changes made."

Respectfully submitted,

Date: December 7, 2001

Brian M. Berliner Attorney for Applicant

Registration No. 34,549

O'MELVENY & MYERS LLP

400 So. Hope Street Los Angeles, California 90071-2899

Telephone: 213-430-6000

VERSION WITH MARKINGS TO SHOW CHANGES MADE

IN THE SPECIFICATION:

Please amend the specification as follows:

On page 5, amend the paragraph starting at line 13 as follows:

[In a development as claimed in claim 7] In an embodiment of the invention, the fluidized-bed gasification chamber is arranged, in spatial terms, above the filter chamber and the filter chamber is arranged above the combustion chamber. This arrangement results in a very compact construction with a good energy balance.

On page 5, amend the paragraph starting at line 20 as follows:

[In a development as claimed in claim 8] In another embodiment of the invention, there is provided an additional heat exchanger, which takes up the waste heat of the drawing-off flue gas and gives it off to the product gas, this likewise improving the energy balance.

On page 5, amend the paragraph starting at line 26 as follows:

[In a development as claimed in claim 9] In another embodiment of the invention, heat-exchanger ribs are arranged on the heat-exchanger sections of the heat pipes. These ribs are formed so as to assume an operative relationship with the streams and vortices of fluid produced by the fluidizing arrangements, such that the fluidized particles are accelerated transversely to their original flow direction. It is thus the case that good transverse mixing of the fluidized bed is achieved, the residence time of the particles in the fluidized bed is increased, gas bubbles are well dispersed, and the heat transfer from the heat-exchanger ribs to the fluidized bed is improved to a considerable extent. This also makes it possible to achieve a compact construction.

On page 6, amend the paragraph starting at line 1 as follows:

A fluidized-bed reactor [as claimed in claim 10] in accordance with the invention is particularly suitable for use in a facility for producing combustible gas from carbon-

containing feed materials according to the present invention. A reactor vessel which accommodates the fluidized bed is provided in the fluidized-bed reactor. Fluidizing arrangements for fluidizing a predetermined region of the fluidized bed are provided. In order for additional heat to be introduced or drawn off in this region, use is made of heat exchangers. The better the heat transfer between the heat exchangers and the fluidized bed, the higher is the efficiency of the installation. In order to improve this heat transfer, the heat-exchanger sections of the heat exchanger are designed as special heat-exchanger ribs which are formed and arranged so as to assume an operative relationship with the streams and vortices of fluid produced by the fluidizing arrangements, such that the fluidized particles are accelerated transversely to their original flow direction, as a result of which the transverse mixing of the fluidized bed is improved, the residence time of the particles in the fluidized bed is increased, and the heat transfer from the heat-exchanger ribs to the fluidized bed is improved to a considerable extent.

On page 7, amend the paragraph starting at line 12 as follows:

[As claimed in claim 13] In another embodiment of the invention, the heat-exchanger ribs are connected releaseably to the heat-exchanger sections. This embodiment has a series of advantages: since, for example, fluidized beds in which combustion processes take place, on account of the relatively high temperature in conjunction with the sand of the fluidized bed, have a highly abrasive effect on internals, the heat-exchanger ribs are particularly effected thereby, i.e. they are subject to a high level of wear. The exchangeability of these parts which are subject to wear is thus particularly cost-effective.

On page 7, amend the paragraph starting at line 24 as follows:

[As claimed in claim 14] In yet another embodiment of the invention, heat pipes are used. It is clear to the person skilled in the art that the positive effect provided by the invention is merely achieved by the particular configuration of the heat-exchanger ribs in conjunction with the fluidized bed. The combination of the special heat-exchanger ribs

with heat pipes again allows a reduced overall size for maintaining the same output.

IN THE CLAIMS:

Please amend the claims as follows:

1. (Amended) A facility for producing combustible gas from carbon-containing [, in particular] biogenic feed materials by allothermic steam gasification, the facility [having the following features] comprising:

a pressure-supercharged fluidized-bed gasification chamber [(10)] with a pressure-tight lock [(2)] for supplying the feed materials [(3) which] that are to be gasified,

a filter chamber [(17) which is] connected to the fluidized-bed gasification chamber [(10)] via a connecting channel [(16, 16')],

an external heat source [(4)], and

a heat-pipe arrangement [(22) which] that takes up heat from the external heat source [(4)] and gives it off to the gasification bed in the fluidized-bed gasification chamber [(10)].

- 2. (Amended) The facility as claimed in claim 1, wherein the external heat source [(4) is a combustion chamber, in particular] <u>further comprises</u> a fluidized-bed combustion chamber [(4)], and has a flue-gas discharge line [(24)].
- 3. (Amended) The facility as claimed in claim 2, wherein the [combustion chamber, in particular the] fluidized-bed combustion chamber [(4),] is connected to the filter chamber [(17)] via a solids flow channel [(19) which] that is directed upward to the filter chamber [(17)],

wherein the solids flow channel [(19)] has a bottom end section [(19a) which is] connected to the combustion chamber [(4)],

wherein the solids flow channel [(19)] has a top end section [(19b) which is] connected to the filter chamber [(17)], and

wherein a siphon arrangement is arranged at the bottom end section [(19a)].

- 4. (Amended) The facility as claimed in claim 3, wherein a first blowing arrangement [(20)] is arranged in the bottom end section [(19a) in order by means] by use of suction action, in a controlled manner, for solids to be drawn off into the fuel bed of the combustion chamber [(4)] from the filter bed of the filter chamber [(17)], [preferably] with pulsating action.
- 5. (Amended) The facility as claimed in claim [3 or] 4, wherein a second blowing arrangement [(21)] is arranged in the top end section [(19b)] of the solids flow channel [(19)] or in the filter chamber [(17)] in order to rearrange and/or loosen the filter bed of the filter chamber [(17)] in a controlled manner.
- 6. (Amended) The facility as claimed in [one of the preceding claims 2 to 5] <u>claim 2</u>, wherein a flue-gas-regulating arrangement is provided in the flue-gas discharge. line [(24)] in order to adjust the ratio of flue gas to product gas.
- 7. (Amended) The facility as claimed in [one of the preceding claims] <u>claim 1</u>, wherein the fluidized-bed gasification chamber [(10)] is arranged above the filter chamber [(17)] and the filter chamber [(17)] is arranged above the combustion chamber [(4)].
- 8. (Amended) The facility as claimed in [one of the preceding claims] claim 2, [wherein there is provided] <u>further comprising</u> an additional heat exchanger, which takes up the waste heat of the drawing-off flue gas [(24)] and gives it off to the product gas.
- 9. (Amended) The facility as claimed in [one of the preceding claims] <u>claim 1</u>, wherein [the] heat-exchanger sections [(24)] of the [heat pipes (22)] <u>heat-pipe arrangement</u> have heat-exchanger ribs [(23; 25; 34)] which are formed and arranged so as to assume an operative relationship with the streams and vortices of fluid produced by the fluidizing arrangements, such that [the] fluidized particles [(28)] are accelerated transversely to their original flow direction, as a result of which [the] transverse mixing of

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the fluidized bed is improved, the residence time of the particles in the fluidized_bed is increased, gas bubbles [(30)] are well dispersed, and [the] heat transfer from the heat-exchanger ribs [(23; 25; 34)] to the fluidized_bed [(26)] is improved to a considerable extent.

10. (Amended) A fluidized-bed reactor, [in particular for a facility as claimed in one of the preceding claims, having] comprising:

a reactor vessel [(7; 36)] for accommodating a fluidized bed [(26)], which is fluidized in a region by <u>fluidizing</u> means [of fluidizing arrangements (38, 40, 42)], and

heat exchangers [(22)] with heat-exchanger sections [(24) which are] arranged in the fluidized region, wherein heat-exchanger ribs [(23; 25; 34)] are formed and arranged on the heat-exchanger sections [(24)] of the heat exchangers [(22)] so as to assume an operative relationship with the streams and vortices of fluids produced by the fluidizing means [arrangements (38, 40, 42)], such that the fluidized particles [(28)] are accelerated transversely to their original acceleration direction, as a result of which the transverse mixing of the fluidized bed [(26)] is improved, the residence time of the fluidized particles [(28)] in the fluidized bed [(26)] is increased, gas bubbles [(30)] are well dispersed, and the heat transfer from the heat-exchanger ribs [(23; 25; 34)] to the fluidized bed [(26)] is improved to a considerable extent.

- 11. (Amended) The fluidized-bed reactor as claimed in claim 10, wherein the heat-exchanger ribs [(23; 25; 34)] are of helical or blade-like design.
- 12. (Amended) The fluidized-bed reactor as claimed in claim 10, wherein, on horizontally located heat-exchanger sections [(24)], the heat-exchanger ribs [(24)] are inclined obliquely to the blowing direction of the fluidizing [arrangement (38, 40, 42)] means, the direction of inclination of the heat-exchanger ribs [(34)] differing from adjacent heat-exchanger sections [(24)].
- 13. (Amended) The fluidized-bed reactor as claimed in [one of the preceding claims 10 to] claim 12, wherein the heat-exchanger ribs [(23; 25; 34)] are connected

releaseably to the heat-exchanger sections [(24)], the connection providing good heat transfer.

14. (Amended) The fluidized-bed reactor as claimed in [one of the preceding claims 10 to 13] claim 10, wherein the heat exchangers [(22)] have heat pipes.

WO 00/77128

PCT/EP00/05364

Facility for the gasification of carbon-containing feed materials

invention The relates to facility a for the gasification of carbon-containing feed materials, e.g. tar, tar sand, plastics waste, residues from paper and pulp production, residues from the petrochemical industry, electronics scrap and light shredded fractions, in particular and of biogenic feed 10 materials, e.g. harvest waste, energy plants (Mishanthus) or wood chips. The facility serves, in particular, for producing combustible gases with a calorific value of at least 8 000 to 10 000 kJ/m^3 .

The energy-related utilization of the abovementioned feed materials, at present, is largely limited to combustion. The gasification technologies are set up predominantly for producing weak gases with a calorific value of below 6 000 kJ/kg. These gases, however, are not suitable for utilization, for example, in gas turbines or fuel cells.

In order to produce gases with a calorific value of $8\,000$ to $10\,000\,\,\mathrm{kJ/m^3}$, so-called allothermic gasification has to be carried out. For this purpose, it is necessary for the fuel which is to be gasified to be fed sufficient external heat at a high temperature level of 500 to 900 degrees Celsius, which up until now has involved high technical outlay.

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A significant widely used gasification process is the fluidized-bed process. This process may also be used to operate relatively small installations costeffectively, but does not produce any high-calorie gases. For allothermic gasification in fluidized beds, essentially the following processes and facilities are currently undergoing testing.

Batelle gasifier

Batelle gasifier Ιn the the of (two-stage fluidized-bed gasification), the reaction heat for the 5 fluidized bed is produced in an external fluidized-bed combustion operation. The heat is transmitted by exchange of the hot sand bed and thus involves high outlay, technical see Peter Jansen, Thermische nachwachsenden Roh- und Vergasung von organischen [Thermal gasification of renewable raw 10 Reststoffen materials and organic residues]; Institutsberichte der Bundesanstalt für Landwirtschaft. [Reports federal institute for agriculture], Brunswick, 1997.

15 DMT gasifier

In the DMT gasifier, a considerable amount of the heat which is necessary for the gasification is to be in that use is made of steam, introduced temperature of 750°C, which is superheated for the 20 fluidizing operation. In addition, for the gasification of biomass, the intention is for heat-exchanger pipes to be directed through the fluidized bed, the flue gas with a temperature of 1 150°C flowing through said pipes. It is barely possible, with the current state of 25 knowledge, to verify that this facility can achieve calorific values approximately 10 000 kJ/kg. of Facilities which operate by this principle disclosed in US 5,064,444 and US 5,439,491.

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In order to increase the chemical conversion, attempts have thus been made to increase the introduction of heat into the fluidized bed by the use of pulse combustors, as is disclosed in US 5,306,481. This method basically allows a relatively high level of heat introduction and thus a chemical conversion which is necessary for allothermic gasification. The use of pulse combustors, however, involves relatively high outlay.

Furthermore, US 4,160,720 discloses a facility which is intended for the gasification of tar sand and in the case of which heat is transmitted into the reaction chamber by means of heat pipes. In the case of this facility, the tar sand runs through the reaction bed and the combustion zone. Since the pyrolysis gas mixes with the flue gas, there is a reduction in the calorific value of this gas, which is not suitable for direct use for gas turbines or for fuel cells.

It is thus an object of the invention to provide a facility for the gasification of carbon-containing and, in particular, biogenic feed materials which ensures a straightforward design and reliable operation and by means of which it is possible to produce combustible gases with a calorific value of at least 8 000 to $10\ 000\ kJ/m^3$. It is also an object of the invention to specify a fluidized-bed reactor which is particularly suitable for such a facility.

The object is achieved by a facility as claimed in claim 1 and by a fluidized-bed reactor as claimed in claim 10.

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A pressure-supercharged fluidized-bed gasification chamber has a pressure-tight lock for supplying the feed materials which are to be gasified. The fluidized-bed gasification chamber is connected to a filter chamber via a connecting channel, with the result that the gas produced can flow over from the fluidized-bed gasification chamber into the filter chamber, where it is directed through the filter layer. An external heat source provides the necessary heat for the allothermic gasification. A heat-pipe arrangement directs the heat from the external heat source into the gasification bed of the fluidized-bed gasification chamber, in order to provide the temperature which is necessary for the gasification.

According to a preferred embodiment of the invention, the external heat is provided by means of combustion, in particular in a fluidized-bed combustion chamber.

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In order that the filter layer does not grow as a of the substances result filtered out combustible gas, some of the growing filter layer is constantly drawn off into the combustion through the solids flow channel. Since the filtered-out substances (ash and residual coke particles) are still combustible in part, they are burned in the combustion chamber. For this purpose, the combustion chamber is preferably connected to the filter chamber via a solids flow channel which is directed upward to the filter chamber. The bottom end section of the solids flow channel has a siphon arrangement in order to deliver material into the combustion chamber from the filter chamber.

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The filter layer is drawn off, according to a further first blowing-out preferred configuration, via a arrangement at the bottom end section of the solids flow channel. In this case, the solids flow channel is preferably 25 vertical. always but inclined and dimensioned such that, when the bottom blowing-out section of the solids flow channel is blown free, the solid material slides downward of its own accord under the action of gravitational force.

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A second blowing-out arrangement is preferably provided at the top end section of the solids flow channel. This serves for rearranging and/or loosening the filter layer.

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Controlling and regulating measures which are known to the person skilled in the art, and specifically the measurement of the gas pressures, determine when and how often the blowing-out arrangement has to be actuated in order to achieve optimum efficiency.

The particular advantage of the invention consists in that, depending on the adjustment of the pressure conditions, either more gas or more flue gas (heat) can be produced. The desired gas/flue gas ratio is preferably adjusted by means of a flue-gas-regulating arrangement, e.g. by the cross section of the flue-gas-outlet channel being changed, it being possible for this to be achieved by a flue-gas damper.

In a development as claimed in claim 7, the fluidized-bed gasification chamber is arranged, in spatial terms, above the filter chamber and the filter chamber is arranged above the combustion chamber. This arrangement results in a very compact construction with a good energy balance.

In a development as claimed in claim 8, there is provided an additional heat exchanger, which takes up the waste heat of the drawing-off flue gas and gives it off to the product gas, this likewise improving the energy balance.

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In a development as claimed in claim 9, heat-exchanger ribs are arranged on the heat-exchanger sections of the heat pipes. These ribs are formed so as to assume an operative relationship with the streams and vortices of fluid produced by the fluidizing arrangements, such that the fluidized particles accelerated are transversely to their original flow direction. It is thus the case that good transverse mixing of the fluidized bed is achieved, the residence time of the fluidized bed is increased, particles in the bubbles are well dispersed, and the heat transfer from the heat-exchanger ribs to the fluidized bed is improved to a considerable extent. This also makes it possible to achieve a compact construction.

A fluidized-bed reactor as claimed in claim 10 is particularly suitable for use in a facility for producing combustible gas from carbon-containing feed materials according to the present invention. A reactor vessel which accommodates the fluidized bed is provided in the fluidized-bed reactor. Fluidizing arrangements for fluidizing a predetermined region of the fluidized bed are provided. In order for additional heat to be introduced or drawn off in this region, use is made of 10 heat exchangers. The better the heat transfer between the heat exchangers and the fluidized bed, the higher is the efficiency of the installation. In order to improve this heat transfer, the heat-exchanger sections 15 exchanger designed the heat are as special heat-exchanger ribs which are formed and arranged so as to assume an operative relationship with the streams and vortices of fluid produced by the fluidizing arrangements, such that the fluidized particles are 20 accelerated transversely to their original direction, as a result of which the transverse mixing of the fluidized bed is improved, the residence time of the particles in the fluidized bed is increased, and the heat transfer from the heat-exchanger ribs to the fluidized bed is improved to a considerable extent. 25

By using such a fluidized-bed reactor, smaller and more cost-effective overall sizes are possible, while maintaining the same output, as a result of the improved heat transfer. Such a fluidized-bed reactor may be used both in the combustion chamber and in the combustible-gas reactor of the facility for producing combustible gas from carbon-containing feed materials.

It should be emphasized that it is not possible or expedient to specify specific dimensioning for the special heat-exchanger ribs since the person skilled in the art can only implement such optimization in conjunction with a specific fluidized-bed reactor. It

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is thus possible, in individual cases, to use very specially designed heat-exchanger ribs which, in certain circumstances, may even be designed to be different, asymmetrical, etc. if this results in the abovedescribed deflection of the particles with the associated positive effects.

Preferred forms of the heat-exchanger ribs are claimed in claims 11 and 12. These forms can be produced to good effect.

As claimed in claim 13, the heat-exchanger ribs are connected releaseably to the heat-exchanger sections. This embodiment has a series of advantages: since, for example, fluidized beds in which combustion processes 15 take place, on account of the relatively high temperature in conjunction with the sand of the fluidized bed, have a highly abrasive effect on internals, the heat-exchanger ribs are particularly effected thereby, i.e. they are subject to a high level 20 of wear. The exchangeability of these parts which are subject to wear is thus particularly cost-effective.

As claimed in claim 14, heat pipes are used. It is clear to the person skilled in the art that the positive effect provided by the invention is merely achieved by the particular configuration of the heat-exchanger ribs in conjunction with the fluidized bed. The combination of the special heat-exchanger ribs with heat pipes again allows a reduced overall size for maintaining the same output.

The invention is explained hereinbelow with reference to two exemplary embodiments in conjunction with attached drawings, in which:

Figure 1 shows a sectional illustration of a first embodiment of the invention,

Figure 2 shows a sectional illustration of a second embodiment of the invention,

Figure 3 shows the effect of the top blowing-out nozzle,

Figure 4 shows the effect of the bottom blowing-out nozzle,

Figure 5 shows a perspective illustration of a blade-design heat-exchanger rib on the heat-exchanger section of a heat exchanger,

Figure 6 shows a perspective illustration of a helical heat-exchanger rib,

Figure 7 shows a perspective functional illustration of the heat-exchanger rib according to figure 6, and

Figure 8 shows heat-exchanger ribs which are arranged on horizontally located heat-exchanger sections.

Figure 1 shows a first embodiment of the invention. A first tubular vessel 1 has, at its top end section 1a, 20 a pressure-tight lock 2 for introducing the feed materials 3 which are to be gasified, illustrated symbolically by means of the Provided in the bottom end section 1b of the vessel 1 is a fluidized-bed combustion chamber 4, into which 25 steam- and/or air-mixture feed nozzles project. starting up, i.e. for heating up, a fuel feed nozzle 6 is arranged within the fluidized-bed combustion chamber 4 in order to blow in combustible gas by means of which the fluidized-bed combustion chamber 4 is heated up. 30

A second tubular vessel 7 is arranged concentrically in the vessel 1 and extends from the top end section 1a to the fluidized-bed combustion chamber 4. At its top end 35 section 7a, this vessel 7 is connected in a sealed manner to the outlet of the lock 2. Arranged at the bottom end section 7b of the vessel combustible-gas outlet 8 for discharging the

combustible gas 9 obtained, said outlet not being connected to the interior of the vessel 1.

Arranged in the top section of the vessel 7 is a fluidized-bed gasification chamber 10, which is described hereinbelow.

The fluidized-bed gasification chamber 10 is a tubular vessel 11 which is open at the top. The vessel 11 is arranged such that the feed materials 3 introduced via the lock 2 drop into the vessel 11. A perforated base 12 is arranged at the bottom end section 11a of the vessel 11, and provided therebeneath is a steam inlet nozzle for the introduction of superheated steam.

15 Arranged above the perforated base 12 is a fuel feed nozzle 15, which serves for the introduction of fuel which is required for starting up and, if appropriate, for controlling the gasification.

The fluidized-bed gasification chamber 10 is arranged concentrically in the vessel 7 such that the remaining annular gap 16 has a predetermined cross section.

Arranged in the bottom section of the vessel 7 is a filter chamber 17, which is described hereinbelow.

The filter chamber 17 comprises a wall section 7c of the second tubular vessel 7 and a filter-chamber perforated base 18, which is arranged above the combustible-gas outlet 8. A solids flow channel 19 is of tubular design and extends from the filter chamber 17, through the filter-chamber perforated base 18, into the fluidized-bed combustion chamber 4, the bottom section 19a of the solids flow channel 19 being curved upward. An upwardly directed bottom blowing-out nozzle 20 projects into said section 19a and the functioning of said nozzle will be explained at a later stage in the text. A further, upwardly directed top blowing-out

nozzle 21 is arranged in the top section 19b of the solids flow channel 19.

Heat pipes 22 extend from the fluidized-bed combustion chamber 4, via the filter chamber 17, to the fluidized-bed gasification chamber 10, those end sections of the heat pipes 22 which project into the fluidized-bed combustion chamber 4 taking in heat and the end sections which project into the fluidized-bed gasification chamber 10 giving it off again there, in 10 order to produce the gasification necessary temperature.

In the present example, helical heat-exchanger ribs 23 are arranged at those end sections of the heat pipes 22 15 fluidized-bed which project into the gasification chamber 10, result with the that transverse acceleration is produced by the upwardly directed steam and bed-material flow, this resulting not just in dispersion of resulting bubbles, but also in transverse 20 mixing in the gasifier bed, by means of which there is an increase in the residence time of the fuel particles in the gasifier bed and thus in the conversion during gasification. Furthermore, the heat transfer between the heat-exchanger ribs 23 and the gasifier bed 25 is improved to a considerable extent.

The gasification process is described hereinbelow:

- 30 The gasification fluidized bed with the feed materials 3 is fluidized by superheated steam which is introduced via the perforated base 12, with the result that thorough mixing of the fluidized bed and of the solid fuels introduced via the lock arrangement is ensured.

 35 The basic functioning of fluidized-bed gasification is
- The basic functioning of fluidized-bed gasification is known to the person skilled in the art and will thus not be explained in detail.

The high level of heat transfer from the heat-introduction sections 24 of the heat pipes 22 to the fluidized bed guarantees a high level of heat fluidized-bed gasification the introduction into chamber. A high level of superheating of the steam introduced additionally ensures that it is possible to maintain temperatures between 500°C and 700°C for the pyrolysis and temperatures up to 800°C for gasification in the gasification bed. These temperatures result, first of all, in the release of volatile constituents of the fuels and, finally, in the conversion of the released hydrocarbons (homogenous of steam gasification) the and residual coke (heterogeneous steam gasification). An excess of steam aids the conversion of the previously formed carbon monoxide with steam into carbon dioxide and hydrogen, as a result of which there is an additional increase in fraction of hydrogen which is important utilization in fuel cells.

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The combustible gases 9 formed in the fluidized-bed gasification chamber 10 are directed, in the directions of the combustible-gas arrows 9, through the annular gap 16 into the filter chamber 17, in which first of all particles of coke and ash are separated off. As the combustible gas 9 flows through the filter bed, the combustible gas reacts with not yet converted steam, as a result of which the conversion, assisted by the catalytic action of the residual coke, is further increased.

combustible the gas 9 flows into fluidized-bed combustion chamber 4 via the solids flow channel 19 some flows directly and into the 35 combustible-gas outlet 8 via the filter-chamber perforated base 18 in order to be supplied for external The division of the two streams utilization. by quantities is combustible-gas determined the pressure loss in the combustible gas in the solids flow

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channel 19 and also by the pressure levels which prevail in the filter chamber 17, the line of the combustible-gas outlet 8 and in the fluidized-bed combustion chamber 4.

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Particles of ash and of residual coke are transferred from the filter layer of the filter chamber 17 into the fluidized-bed combustion chamber 4 in that filter-bed material is discharged intermittently from the section 19a of the solids flow channel 19. The blowing-out nozzle is activated for this purpose.

In order for bed material to be discharged from the solids flow channel 19 into the filter layer of the filter chamber 17, steam is blown in via the blowing-out nozzle 21, see figure 3. This achieves the situation where the bed material covers the deposited ash and the residual coke particles in layers.

The combustible gas 9 introduced into the fluidized-bed combustion chamber 4 is burned together with the residual coke fractions and tars separated off in the filter bed. Some of the heat released here is given off to the heat-accommodating sections of the heat pipes 22, which direct the heat to the fluidized-bed gasification chamber 10.

The rest of the heat is discharged from the fluidized-bed combustion chamber 4 with the flue gas 24 as perceived heat and is used outside the facility for producing superheated steam. This superheated steam is guided back wholly or partially into the facility as a gasification and fluidizing means.

In the present embodiment, nozzles 6 and 15 for introducing liquid or gaseous fuels are provided, in addition, in the fluidized-bed combustion chamber 4 and in the fluidized-bed gasification chamber 10. These nozzles serve, in particular, for heating up the

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facility during the starting-up process in order for it to be possible to use, for example, liquid biogenic fuels or in order for it to be possible to utilize liquid fuels or combustible gases which occur in external processes. This is expedient, in particular, when, for example during the operation of fuel cells in conjunction with the gasification facility, hydrogen is separated off in intermediate separating processes and the other constituents contained in the combustible gas (carbon monoxide, methane and higher hydrocarbons) are to be guided back for heat production.

In order to produce hot water, saturated steam or it superheated also possible steam, is for steam-generator pipes to be integrated, e.g. as ribbed heating immersion surfaces, wholly pipes or partially in a fluidized-bed combustion chamber.

It should also be mentioned that the fluidized-bed combustion chamber has a conventional ash-discharge arrangement.

Figure 2 shows a further embodiment of the invention. In this embodiment, the fluidized-bed gasification chamber 10, the filter chamber 17 and the fluidized-bed combustion chamber 4 are arranged one beside the other and are likewise coupled thermally via the heat pipes 22. The same functional elements are provided with the same designations. In the case of functioning which corresponds to the first embodiment, the explanation is not repeated and you are thus referred to the explanation relating to figure 1.

The feed materials 3 which are to be gasified are introduced through the pressure-tight lock 2 and gasified as in the first embodiment. The combustible gas 9 passes, via the channel 16', into the filter chamber 17, flows through the latter and passes out of the combustible-gas outlet 8 in the filtered state.

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Some of the combustible gas is directed through the solids flow channel 19 and burned in the fluidized-bed combustion chamber 4.

As in the first embodiment, blowing-out nozzles 20 and 21 are arranged in the end sections 19a of the solids flow channel 19.

Figure 3 shows the functioning of the top blowing-out nozzle 21. The arrows show how the material is fluidized and rearranged.

Figure 4 shows the functioning of the bottom blowing-out nozzle 20. The arrows show how filter 15 material is drawn off from the filter chamber and is fed to the combustion chamber for combustion purposes.

Finally, it should also be mentioned that it would be possible for the specific way of discharging material by means of the blowing-out nozzles 20 and 21 to be replaced by a mechanical discharge arrangement. Such a discharge arrangement, e.g. conveying screws, however, is/are more expensive than blowing nozzles and is/are susceptible to malfunctioning under the prevailing operating conditions, with the result the solution with the blowing nozzles is preferred.

Different embodiments of heating or cooling ribs on the heat-exchanger sections of the heat pipes are described hereinbelow with reference to figures 5 to 8. These heating and cooling ribs are particularly suitable for the fluidizing-bed reactor according to the present invention thus fluidized-bed and also for the fluidized-bed gasification chamber 10 and the combustion chamber 4.

Figure 5 shows an end section 24 of a heat exchanger, in particular in the form of a heat pipe 22, on which blade-design heat-exchanger ribs 25 are arranged.

Figure 6 shows an end section 24 of a tubular heat exchanger or of a heat pipe 22 on which helical heat-exchanger ribs 23 are arranged.

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Figure 7 shows the tubular end section 24 of a heat exchanger 22 with helical heat-exchanger ribs 23 (such as in figure 6) in a fluidized bed 26 which consists, for example, of fuel particles 28 and in which gas bubbles 30 are rising. The arrows 32 show the direction in which the fuel particles 28 and the gas bubbles 30 are deflected. The fluidized bed 26 is assigned to a reactor vessel which corresponds to the tubular vessel 7 in figure 1. The outer vessel 1 from figure 1 is also illustrated laterally. Figure 7 thus constitutes a detail of figure 1.

The fluidized bed is homogenized by said lateral deflection. At the same time, the fuel particles 28 remain in the fluidized bed longer, with the result that they are burned in their entirety. A longer residence time of the feed materials is also desirable in other reactions, e.g. gasification. The lateral deflection gives the particles very good heat contact with the heat-exchanger ribs 23, as a result of which the heat transfer is improved to a considerable extent and the efficiency is thus increased.

Figure 8 shows part of a fluidized-bed reactor with horizontally located heat-exchanger pipes 22 30 heat-exchanger sections 24, on which heat-exchanger ribs 34 are arranged. The heat-exchanger sections 24 project horizontally into the fluidized bed 26, which is arranged in a reactor vessel 36. The reactor vessel 36 comprises a base plate which is designed as a 35 perforated base 38 with holes 40. A fluidizing arrangement is illustrated by way of the holes 40 together with arrows 42.

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In this embodiment, the heat-exchanger ribs 34 are inclined, direction inclination of the of the heat-exchanger ribs 34 having been changed in the heat-exchanger section 24 located above. The particles and the steam bubbles 30 are thus 28 deflected alternatively to the left or right, which results in good transverse mixing. It is thus clear to the person skilled in the art that the heat-exchanger ribs 34 according to the teaching of the invention are to be provided in the case of heat-exchanger sections 24 which are located obliquely.

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Claims

- 1. A facility for producing combustible gas from carbon-containing, in particular biogenic feed materials by allothermic steam gasification, the facility having the following features:
 - a pressure-supercharged fluidized-bed gasification chamber (10) with a pressure-tight lock (2) for supplying the feed materials (3) which are to be gasified,
- a filter chamber (17) which is connected to the fluidized-bed gasification chamber (10) via-a connecting channel (16, 16'),
 - an external heat source (4), and
- a heat-pipe arrangement (22) which takes up heat from the external heat source (4) and gives it off to the gasification bed in the fluidized-bed gasification chamber (10).
- 20 2. The facility as claimed in claim 1, wherein the external heat source (4) is a combustion chamber, in particular a fluidized-bed combustion chamber (4), and has a flue-gas discharge line (24).
- 25 3. The facility as claimed in claim 2, wherein the combustion chamber, in particular the fluidized-bed combustion chamber (4), is connected to the filter chamber (17) via a solids flow channel (19) which is directed upward to the filter chamber (17),
 - wherein the solids flow channel (19) has a bottom end section (19a) which is connected to the combustion chamber (4),
- wherein the solids flow channel (19) has a top end section (19b) which is connected to the filter chamber (17), and
 - wherein a siphon arrangement is arranged at the bottom end section (19a).

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- 4. The facility as claimed in claim 3, wherein a first blowing arrangement (20) is arranged in the bottom end section (19a) in order by means of suction action, in a controlled manner, for solids to be drawn off into the fuel bed of the combustion chamber (4) from the filter bed of the filter chamber (17), preferably with pulsating action.
- 10 5. The facility as claimed in claim 3 or 4, wherein a second blowing arrangement (21) is arranged in the top end section (19b) of the solids flow channel (19) or in the filter chamber (17) in order to rearrange and/or loosen the filter bed of the filter chamber (17) in a controlled manner.
 - 6. The facility as claimed in one of the preceding claims 2 to 5, wherein a flue-gas-regulating arrangement is provided in the flue-gas discharge line (24) in order to adjust the ratio of flue gas to product gas.
- 7. The facility as claimed in one of the preceding claims, wherein the fluidized-bed gasification chamber (10) is arranged above the filter chamber (17) and the filter chamber (17) is arranged above the combustion chamber (4).
- 8. The facility as claimed in one of the preceding claims, wherein there is provided an additional heat exchanger, which takes up the waste heat of the drawing-off flue gas (24) and gives it off to the product gas.
- 35 9. The facility as claimed in one of the preceding claims, wherein the heat-exchanger sections (24) of the heat pipes (22) have heat-exchanger ribs (23; 25; 34) which are formed and arranged so as to assume an operative relationship with the

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streams and vortices of fluid produced by the fluidizing arrangements, such that the fluidized particles (28) are accelerated transversely to their original flow direction, as a result of which the transverse mixing of the fluidized bed is improved, the residence time of the particles in the fluidized bed is increased, gas bubbles (30) are well dispersed, and the heat transfer from the heat-exchanger ribs (23; 25; 34) to the fluidized bed (26) is improved to a considerable extent.

- 10. A fluidized-bed reactor, in particular for a facility as claimed in one of the preceding claims, having
 - a reactor vessel (7; 36) for accommodating
 - a fluidized bed (26), which

to a considerable extent.

- is fluidized in a region by means of fluidizing arrangements (38, 40, 42), and
- (22) with heat-exchanger exchangers 20 heat sections (24) which are arranged in the fluidized region, wherein heat-exchanger ribs (23; 25; 34) are formed and arranged on the heat-exchanger sections (24) of the heat exchangers (22) so as to assume an operative relationship with the streams 25 and vortices of fluids produced by the fluidizing arrangements (38, 40, 42), such that the fluidized particles (28) are accelerated transversely to their original acceleration direction, as a result of which the transverse mixing of the fluidized 30 bed (26) is improved, the residence time of the fluidized particles (28) in the fluidized bed (26) is increased, gas bubbles (30) are well dispersed, and the heat transfer from the heat-exchanger ribs (23; 25; 34) to the fluidized bed (26) is improved 35

- 11. The fluidized-bed reactor as claimed in claim 10, wherein the heat-exchanger ribs (23; 25; 34) are of helical or blade-like design.
- 5 12. The fluidized-bed reactor as claimed in claim 10, wherein, on horizontally located heat-exchanger sections (24), the heat-exchanger ribs (24) are inclined obliquely to the blowing direction of the fluidizing arrangement (38, 40, 42), the direction of inclination of the heat-exchanger ribs (34) differing from adjacent heat-exchanger sections (24).
- 13. The fluidized-bed reactor as claimed in one of the preceding claims 10 to 12, wherein the heat-exchanger ribs (23; 25; 34) are connected releaseably to the heat-exchanger sections (24), the connection providing good heat transfer.
- 20 14. The fluidized-bed reactor as claimed in one of the preceding claims 10 to 13, wherein the heat exchangers (22) have heat pipes.

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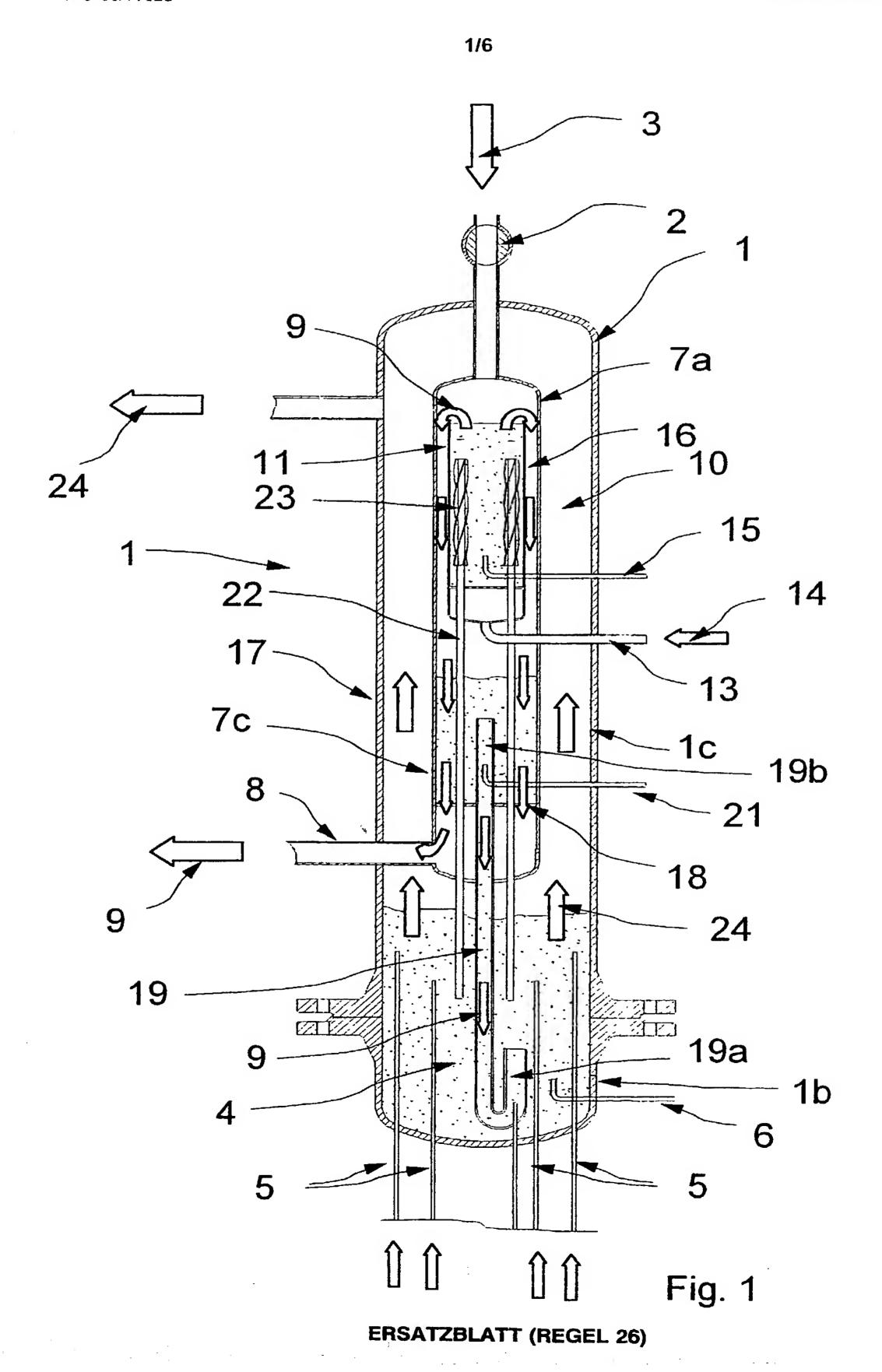
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Zur Erklärung der Zweibuchstaben-Codes, und der anderen Abkürzungen wird auf die Erklärungen ("Guidance Notes on Codes and Abbreviations") am Anfang jeder regulären Ausgabe der PCT-Gazette verwiesen.

- (54) Title: DEVICE FOR THE GASIFICATION OF CARBONACEOUS FEEDSTOCK
- (54) Bezeichnung: VORRICHTUNG ZUR VERGASUNG KOHLENSTOFFHALTIGER EINSATZSTOFFE
- (57) Abstract: The invention relates to a device for the gasification of carbonaceous and especially biogenic feedstock that allows a simple design and safe functioning. The invention also provides a fluidized reactor to be used together with said device. According to the invention, the pressurized fluid bed gasification chamber comprises a pressure-resistant lock-chamber for charging the feedstock to be gasified. The fluid bed gasification chamber is linked with a filter chamber via a connection channel so that the gas issued from the fluid bed gasification chamber can flow into the filter chamber where it is passed through the filter layer. An external heat source provides the heat required for the allothermic gasification. The heat is guided from the external heat source to the gasification bed of the fluid bed gasification chamber by means of a thermoconductive tube system and provides the temperature required for the gasification process.
- (57) Zusammenfassung: Es wird eine Vorrichtung zur Vergasung von kohlenstoffhaltigen und insbesondere biogenen Einsatzstoffen bereitgestellt, die eine einfache Konstruktion und sichere Arbeitsweise gewährleistet. Außerdem wird ein hierfür geeigneter Wirbelschichtreaktor angegeben. Gemäß der Erfindung umfaßt eine druckaufgeladene Wirbelschichtvergasungskammer eine druckfeste Schleuse zur Aufgabe der zu vergasenden Einsatzstoffe. Die Wirbelschichtvergasungskammer ist mit einer Filterkammer über einen Verbindungskanal verbunden, so daß das entstehende Gas von der Wirbelschichtvergasungskammer in die Filterkammer überströmen kann, wo es durch die Filterschicht geleitet wird. Durch eine externe Wärmequelle wird die für die allotherme Vergasung notwendige Wärme bereitgestellt. Mittels einer Wärmeleitrohranordnung wird die Wärme aus der externen Wärmequelle in das Vergasungsbett der Wirbelschichtvergasungskammer geleitet, um die für die Vergasung erforderliche Temperatur bereitzustellen.





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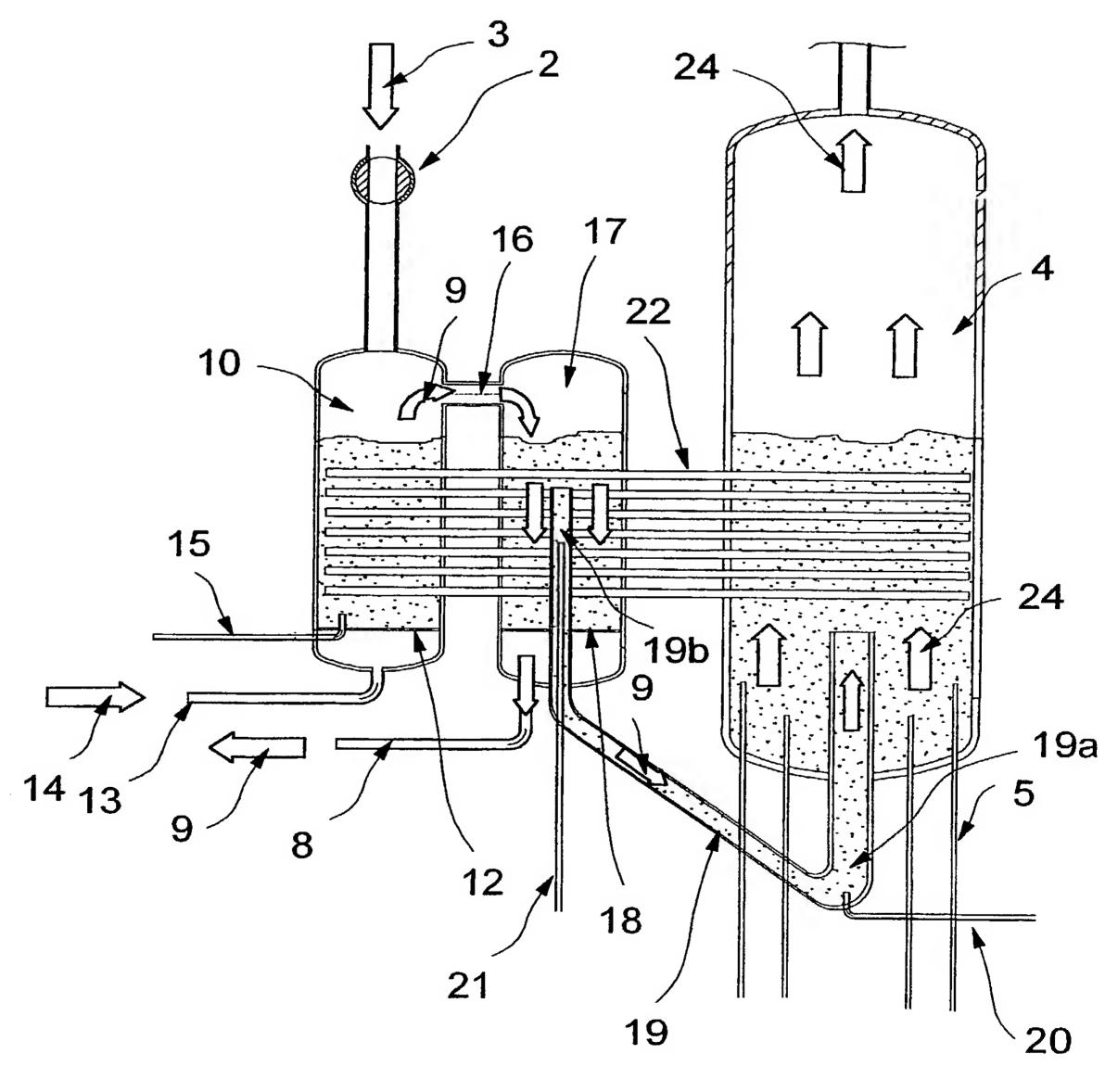


Fig. 2

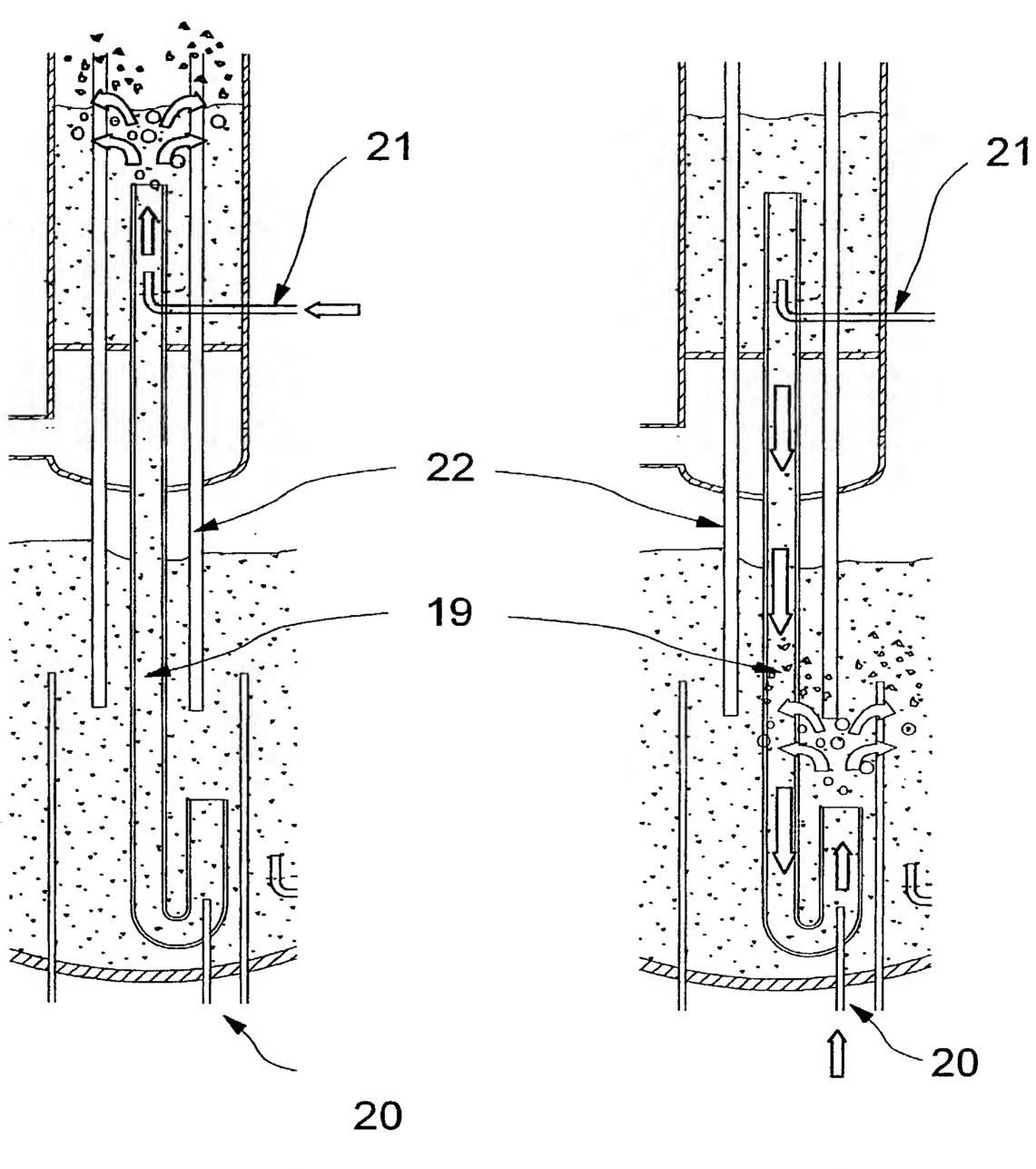


Fig. 3

Fig. 4

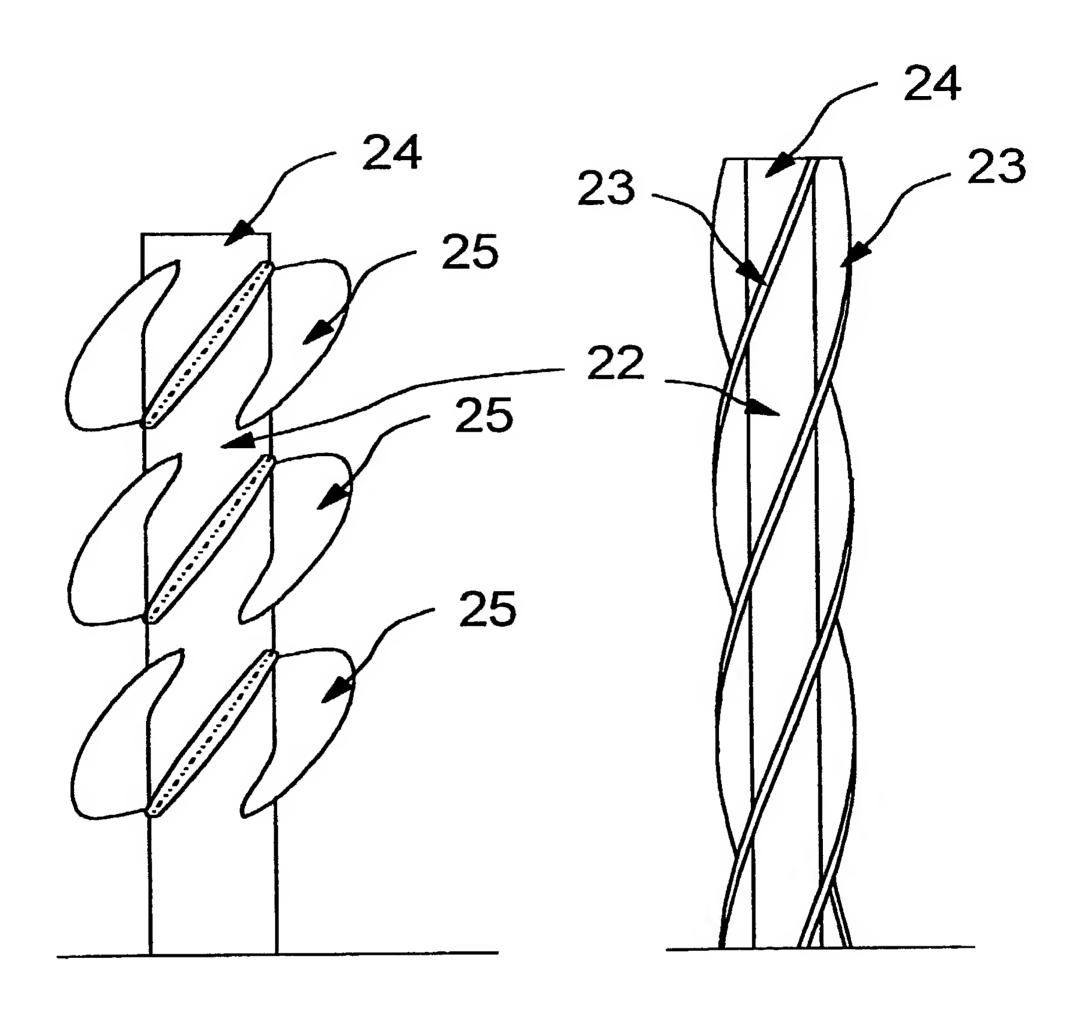


Fig. 5

Fig. 6

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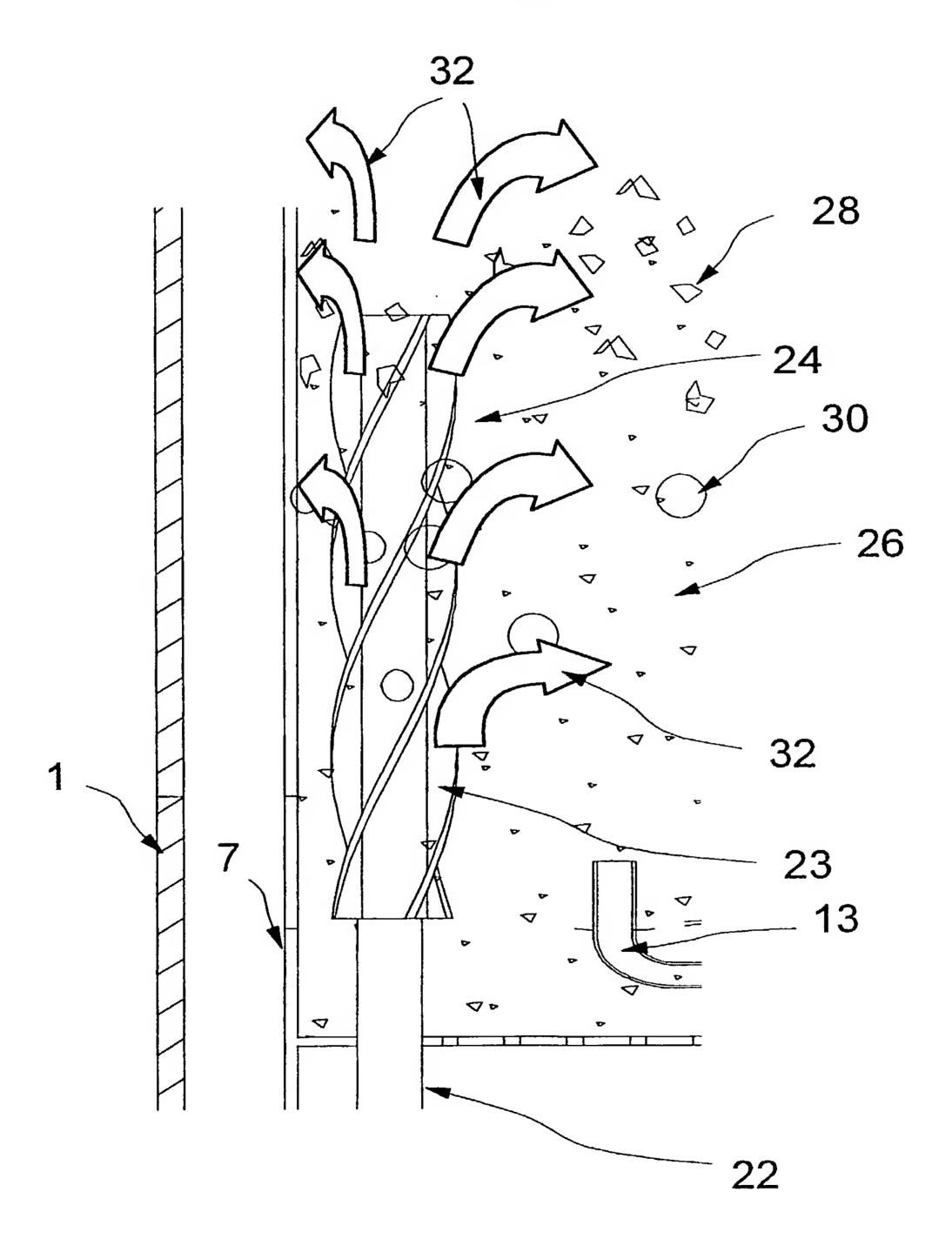
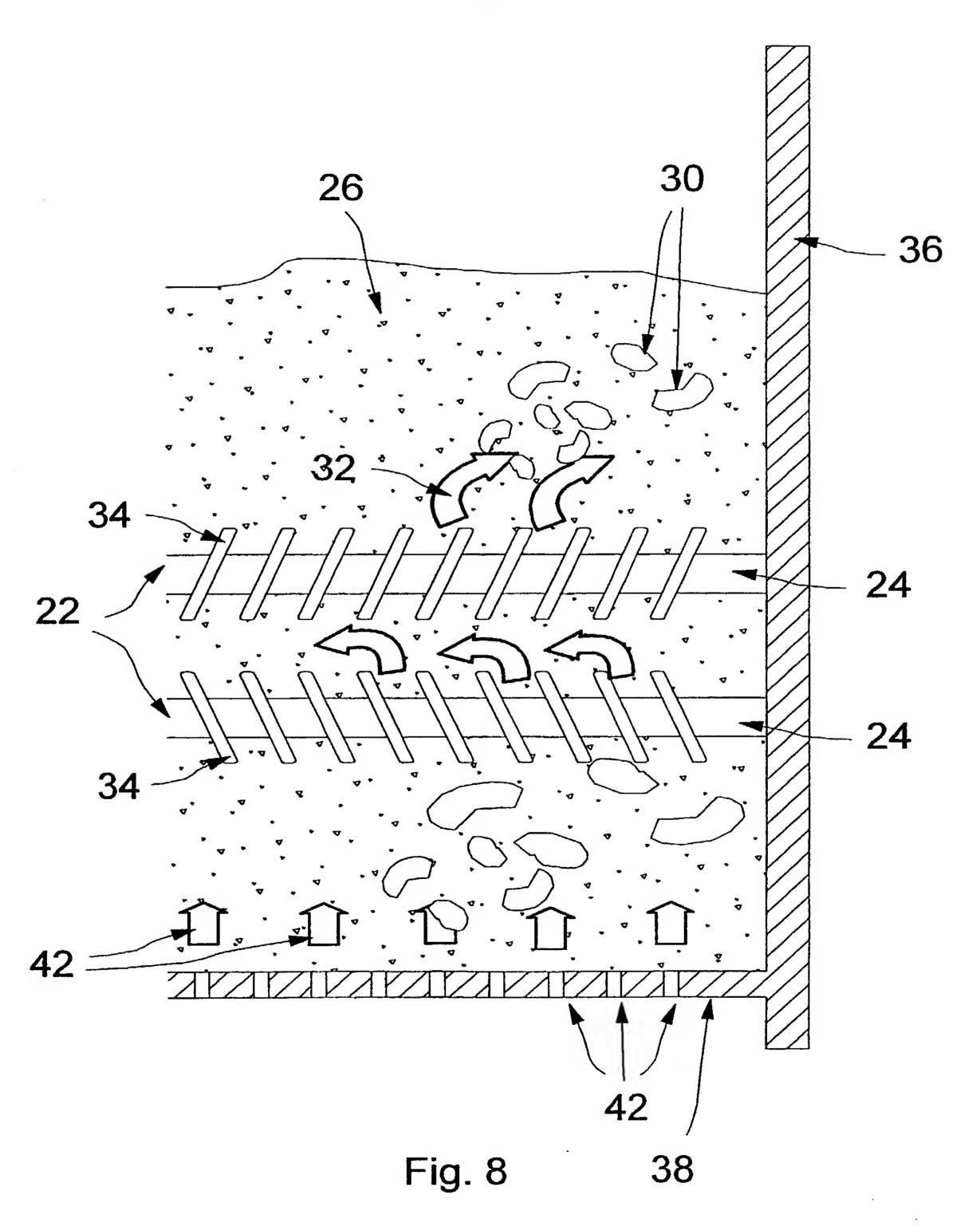


Fig. 7
ERSATZBLATT (REGEL 26)

WO 00/77128

PCT/EP00/05364



☐ YES

□ NO

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COMBINED DECLARATION FOR PARTICULATION AND POWER OF AT (Includes Reference to PCT International Applications)		torney's Docket Nu 2640-18	olp E	U.S. Application No. (10/009/542	ıf known):	
•			8			
As a below named inventor, I hereby dec			JAN 0 3 5005 F	!)		
ly residence, post office address and citize		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	ame,	/		
believe I am the original, first and sole invene subject matter which is claimed and for v	ntor (if only one name which a patent is soug	e is listed below) of ght on the invention	entitled:	nd joint inventor (if plura	I names are lis	sted below) of
FACILITY FOR THE GASIFICATION OF CA	ARBON-CONTAININ	G FEED MATERIA	NLS			
ne specification of which						
☐ is attached hereto						
OR						
■ was filed as United States Application	Number or PCT Inter	national Application	n Number			
10/009,542	,	, , , , , , , , , , , , , , , , , , ,				
on December 7, 2001						
and was amended						'
on (if	applicable)					
hereby state that I have reviewed and undermendment referred to above. acknowledge the duty to disclose information acknowledge the duty to disclose information acknowledge.						
hereby claim the benefit under Title 35, Unit	ted States, §119 (e) (of any United State	s provisional applic	cation(s) listed below		
Application Number) .	(Filing Date)				
Application Number)	(Filing Date	9)				
hereby claim foreign priority benefits under certificate or §365 (a) of any PCT internationand have also identified below any foreign apperfore that of the application(s) of which prior	al application(s) whic oplication(s) for paten	h designated at lea	ast one country oth	er than the United State	s of America,	listed below
RIOR FOREIGN/PCT APPLICATION(\$) AN	ID ANY PRIORITY C	LAIMS UNDER 35	U S.C. 119:			
COUNTRY (if PCT, indicate "PCT")	APPLICATION	NUMBER		OF FILING nonth, year)	PRIORITY UNDER 35	
ermany	DE 19926202.0		09 June 1999		■ YES	□ NO
ermany D	DE 19926201.2		09 June 1999		≥ YES	□ NO
ermany	DE 19926203 9		09 June 1999		☑ YES	□ NO
CT P	PCT/EP00/05364		09 June 2000		☑ YES	□ NO
*					☐ YES	□ NO

Combined Declaration For Patent Application and Power of Attorney
(Continued)

(RADEMARIO)

ATTORNEY'S DOCKET NUMBER 942640-18

I hereby claim the benefit under Title 35, United States Code, §120 of any United States application(s) or §365 of any PCT international application(s) designating the United States of America that is/are listed below and, insofar as the subject matter of each of the claims of this application is not

l disci	iose material informa	mon as u	efined in Title 37, Code of Fednal filing date of this application	ed by the first paragraph of Title 38 leral Regulations, §1.56 which occors:	curred betw	een the filing date of the	prior application(s)		
PRIC	OR U.S. APPLICATI	ONS OR	PCT INTERNATIONAL APPL	ICATIONS DESIGNATING THE L	J.S. FOR B	SENEFIT UNDER 35 U.S.	C. 120:		
U.S. APPLICATIONS						STATUS (Check one)			
U.S. APPLICATION NUMBER				U S FILING DATE	PATE	NTED PENDING	ABANDONED		
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		PCT AF	PLICATIONS DESIGNATING	THE U.S.					
PCT APPLICATION NO			PCT FILING DATE U.S. SERIAL NUMBERS ASSIGNED (if any)						
Todd ,45,57 Send Brian O'MI 400	sact all business in E. Fitzsimmons, Reg. No ;	the Pate 44,683, Der n of O'MEL\ to:	nt and Trademark Office co inis R Gallagher, Reg No. 42,563, Jo /ENY & MYERS LLP, 400 So Hope S	oint the following attorney(s) an nnected therewith. (List name ai nathan A Jaech, Reg No 41,091, Ryan K street, Los Angeles, CA 90071-2899	nd registrat	IOD DUMber) Brian M. Berline	r, Reg No 34,549, n, Reg No		
	FAMILY NAME FULL NAME OF KARL		FIRST GIVEN NAME JURGEN			SECOND GIVEN NAME			
100	INVENTOR	TOTAL .		JONGEN					
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2 0 2	FULL NAME OF INVENTOR	FAMILY	NAME	FIRST GIVEN NAME		SECOND GIVEN NAME			
-	RESIDENCE & CITIZENSHIP	CITY		STATE OR FOREIGN COUNTRY	STATE OR FOREIGN COUNTRY		COUNTRY OF CITIZENSHIP		
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2 0	FULL NAME OF INVENTOR	FAMILY	NAME	FIRST GIVEN NAME		SECOND GIVEN NAME			
3	RESIDENCE & CITIZENSHIP	CITY		STATE OR FOREIGN COUNTRY	STATE OR FOREIGN COUNTRY		COUNTRY OF CITIZENSHIP		
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be tru imprii applie	ue; and further that the sonment, or both, un cation or any patent	hese state ider section issung th	ements were made with the ki on 1001 of Title 18 of the Unit greon.	wledge are true and that all statem nowledge that willful false stateme ed States Code, and that such will	nts and the ful false sta	like so made are punish atements may jeopardize	able by fine or		
SIGNATURE OF INVENTOR 201 SIGNATURE OF INVENTOR 202 SIGNATURE OF INVENTOR 203									
DATE خونہ	7.5,2002	11	DATE		DATE				
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KRAFTANLAGEN MIT HEIZKRAFTWERK Prof Dr.-Ing D. Hein TECHNISCHE UNIVERSITAT MUNCHEN

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